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A Proposed Standard Climate for Evaluating Rocket Exhaust Secondary Smoke Formation and Visibility Revision 1
Andrew C./Victor  Advanced Technology Division  Ordnance Systems Department
WC-TM-3638-REV-ユ) January 1979
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### **FOREWORD**

This report presents the results of work which was supported by the Naval Air Systems Command, "Advanced Reliable Solid Propulsion Design," Propulsion Administrators, Mr. Robert Heitkotter (NAVAIR) and Dr. Charles Thelen (NWC) and by the Naval Sea Systems Command, "Plume Low Signature Requirements for Point/Area Defense Solid Propellant Motors," J. Murrin and R. Cassel. The Program Manager was Mr. George Buckle, Naval Ordnance Station, Indian Head, MD.

This report is a revision of NWC TM 3638. Since the original report was published in November 1978, an error in the computer program that was used to generate much of the data in the report has been corrected. As a result, Tables 2 throught 15 and the computer program in the Appendix have been changed. Also, a slight change has been made in the percent value in Figure 4.

This report is issued for use at the working level only and does not reflect an official position of the Naval Weapons Center.

Duane H. Williams Head, Advanced Technology Division Ordnance Systems Department 28 January 1979

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### **NWC TM 3638**

### **ABSTRACT**

Under certain climatic conditions rocket motor exhaust plumes can form contrails which are highly visible at long ranges. It is difficult to predict accurately the formation and visibility of these contrails unless the important climatic factors (temperature and moisture content) are known. This report proposes a preliminary definition of a climate at 40°N and 50°N latitude for altitudes from 2-15 km based on a review of relevant literature. Both temperature and moisture content are expressed in terms of mean values and standard deviations so that the probability of occurrence of any climatic conditions can be estimated.

### INTRODUCTION

Moisture laden exhaust contrails can greatly increase the detectability of missiles and aircraft. The problem is most severe for those rocket motors which contain, as products of combustion, water soluble gas and particle species which increase the propensity for moisture condensation. Therefore, avoidance of contrail formation is an important design criterion for certain missions required of modern missile propulsion systems. Changes made in missile propellant ingredients in order to meet this criterion often result in reduced rocket motor total energy. To minimize this compromise of motor energy it is important, in the system design phase, to perform trade-off analyses of the effects of energy and contrail formation on the performance of a missile's mission.

Previous studies have yielded techniques for predicting missile performance<sup>1</sup> and the visibility of primary smoke\* trails. Although techniques have also been developed for predicting the formation and visibility of secondary smoke\*\* contrails<sup>3,4</sup>, these predictions require inclusion of ambient temperature and humidity values.

Temperature and humidity values needed for incorporation in contrail predictions may be obtained in several ways:

- 1. Use specific values based on specific measurements
- 2. Use standard climatic values<sup>5,6</sup>

<sup>\* &</sup>quot;Primary smoke" is composed of the solid effluent from propulsion systems.

<sup>\*\* &</sup>quot;Secondary smoke" is formed by condensation of plume and atmospheric water on the microscopic particle efflux; it often contains water soluble species too.

<sup>1</sup> Naval Weapons Center. Tactical Missile Encounter (TAME) Simulation Computer Program, by D. R. Peters, R. D. Feldman, H. Sobel and M. J. Stevens. China Lake, Calif., NWC, March 1970. (NWC TP 4866, publication IINCLASSIFIED.)

publication UNCLASSIFIED.)

<sup>2</sup> A. C. Victor and S. H. Breil. "A Simple Method for Predicting Rocket Exhaust Smoke Visibility," J SPACECRAFT AND ROCKETS, Vol. 14, No. 9 (September 1977), pp. 526-533.

<sup>&</sup>lt;sup>3</sup> Naval Weapons Center, "Computer Codes for Predicting Secondary Smoke Formation in Free Jets and Smoke Chambers," by A. C. Victor. China Lake, Caiff., NWC, February 1978. (NWC TM 3361, publication UNCLASSIFIED.)

<sup>&</sup>lt;sup>4</sup> H. Hoshizaki, et. al. "Plume Visibility Detection Study," presented at the 10th JANNAF Plume Technology Meeting, 14-17 September 1977. (NWC TM 3361, publication UNCLASSIFIED.)

U.S. Standard Atmosphere 1962. U.S. Government Printing Office, December 1972, Washington, D.C.
 Air Force Cambridge Research Laboratories, Handbook of Geophysics and Space Environments, S. L.
 Valley, Ed. Bedford Mass., 1965, Chapter 3. (UNCLASSIFIED.)

- 3. Use tabulated climatic values (footnotes 5 and 6) and make the contrail predictions for a world-wide, year round, range of climates
- 4. Use a statistically defined climate model (humidity, temperature, altitude) which corresponds to observations and makes the contrail prediction at statistically significant points in the climate

Each of these methods of selecting climatic values has distinct advantages and disadvantages. The first method is useful only to verify the predictive technique by comparison with previously made measurements; it has no relevance for system design studies.

The second method is useful for a quick look approach, but it cannot provide probabilities of contrail formation which are needed in the design study.

The third method is capable of generating the predictions needed in design studies, but at an excessive cost, because of the many climate conditions involved. This method is most useful for evaluating contrail formation in specific operation theaters.

The fourth method is essentially a condensation of the third method in that weather statistics are included in the climate model. Thus with only a few calculations the probability of contrail formation for a specific missile propulsion system can be predicted as a function of altitude and latitude.

This report presents a simple model climate based on the fourth method above, which averages annual climate variations at specific latitudes. Latitudes of 40°N and 50°N were chosen as being typical of the United States and Western Europe, respectively.

A more complex statistical model, based on accumulated world-wide statistics, although desirable, was beyond the manpower and funding limits of the projects which supported this study. Such a model would be capable of predicting weather probabilities on any specific date, whereas the model described in this report can only predict probabilities for an arbitrary date.

### **CLIMATE MODEL**

The climate model needed for contrail prediction has four elements:

- 1. Mean temperature as a function of altitude
- 2. Standard deviation of temperature as a function of altitude
- 3. Mean humidity as a function of altitude
- 4. Standard deviation of humidity as a function of altitude

### **TEMPERATURE MODEL**

Temperature as a function of altitude has been measured carefully for many years, and sufficient data are reported to define both elements 1 and 2 above. From Table 3-9 in *Handbook of Geophysics and Space Environments* (footnote 6), Equations 1 and 2 have been generated to represent mean annual temperature, in degrees Celsius, at 40°N and 50°N latitude respectively, as functions of altitude (y) in km up to 20 km.

$$T_{40^{\circ}N} = 28.56 - 10.618y + 0.3168y^2$$
 (1)

$$T_{50^{\circ}N} = 12.95 - 8.774y + 0.2738y^2$$
 (2)

Equations 3 and 4 represent the January and July mean variations of temperature about the annual mean:

$$t_{40}^{\circ}N = 8.0 - 0.56y + 0.0153y^2$$
 (3)

$$t_{50}^{\circ}N = 10.3 - 0.7y + 0.0167y^2$$
 (4)

The mean temperature in January and July are given by:

$$T(jan)_{40} \circ_{N} = T_{40} \circ_{N} - t_{40} \circ_{N} \qquad 0 \text{ to } 12 \text{ km altitude}$$

$$= T_{40} \circ_{N} + t_{40} \circ_{N} \qquad 14 \text{ to } 20 \text{ km}$$

$$= T_{40} \circ_{N} + t_{40} \circ_{N} \qquad 12 \text{ to } 14 \text{ km}$$

$$T(july)_{40} \circ_{N} = T_{40} \circ_{N} + t_{40} \circ_{N} \qquad 0 \text{ to } 12 \text{ km}$$

$$= T_{40} \circ_{N} - t_{40} \circ_{N} \qquad 14 \text{ to } 20 \text{ km}$$

$$= T_{40} \circ_{N} \qquad 12 \text{ to } 14 \text{ km}$$

$$T(jan)_{50} \circ_{N} = T_{50} \circ_{N} - t_{50} \circ_{N}$$

$$T(july)_{50} \circ_{N} = T_{50} \circ_{N} + t_{50} \circ_{N} \qquad 0 \text{ to } 20 \text{ km}$$

The standard deviations ( $\sigma$ ) about the January and July mean values (up to 15 km) are approximately:

$$\sigma(\text{jan})_{40^{\circ}\text{N}} = \pm 5^{\circ}\text{C}$$

$$\sigma(\text{july})_{40^{\circ}\text{N}} = \pm 3^{\circ}\text{C}$$

$$\sigma(\text{jan})_{50^{\circ}\text{N}} = \pm 6^{\circ}\text{C}$$

$$\sigma(\text{july})_{50^{\circ}\text{N}} = \pm 4^{\circ}\text{C}$$

Therefore upper and lower likely (1 $\sigma$ ) extremes of temperature are given approximately by

$$T_{+} = T + t + \sigma(\text{july}) \tag{5}$$

$$T_{-} = T - t - \sigma(jan) \tag{6}$$

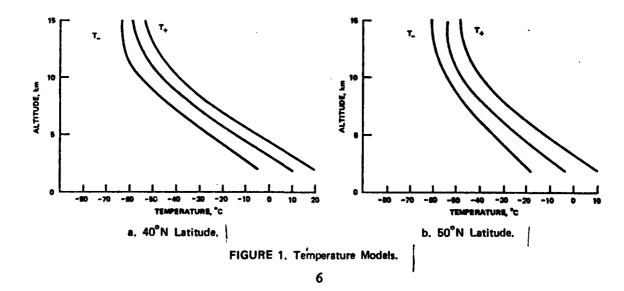
except at 40°N latitude above 14 km where the upper extreme is given by:

$$T_{+} = T + t + \sigma(jan) \tag{7}$$

and lower by:

$$T_{-} = T - t - \sigma(july)$$
 (8)

The temperature models are shown graphically in Figure 1. The mathematical models defined by Equations 1 through 8 are not intended for use outside the altitude range 2-15 km.



### **HUMIDITY MODEL**

The information in footnote 6 and more recent measurements<sup>7</sup> show that mean atmospheric moisture content can be well represented by Equation 9 for the mixing ratio W = mass of atmospheric water/mass air, in parts per million,

$$W = 10^{(3.7 - 0.192y)}$$
 for 0-10 km altitude  
=  $10^{4.13 - 0.235y}$  for 10-15 km altitude (9)

up to an altitude of 15 km (about 50,000 feet). The data in footnote 7 indicate that the fractional standard deviation about the means is about 0.6 at all altitudes.

The actual water vapor pressure  $(e_v)$  is obtained from the mixing ratio by Equation 10

$$e_{v} = \frac{PW \times 10^{-6}}{0.622 + W \times 10^{-6}} \cong \frac{PW}{0.622 \times 10^{6}}$$
 (10)

in the units of atmospheric pressure (P).

Standard atmospheric pressure (footnote 6) as a function of altitude is given in Table 1.

TABLE 1. Atmospheric Pressure  $(P)^a$  as a Function of Altitude (y).

y, km	P, mb	y, km	P, mb
0	1013	12	193
2	795	14	141
4	616	16	103
6	472	18	75.0
8	356	20	54.7
10	264	22	40.0

<sup>&</sup>lt;sup>4</sup> The following constants may be used to convert to other pressure units:

mb x 0.00098692 = atmospheres

mb  $\times 10^8$  = pascals (N m<sup>-2</sup>)

 $mb \times 0.014504 = pounds/inch^2$ 

mb x 0.7502 = mm of mercury at 0°C

<sup>&</sup>lt;sup>7</sup> Air Force Cambridge Research Laboratories, "Humidity Up to the Mesopause," by N. Sissenwine, D. D. Granthan and H. A. Samela, Bedford, Mass., October 1968. (AFCRL-68-0530, AD 679996, UNCLASSIFIED.)

By combining Equations 9 and 10, Table 1, and water vapor pressure curves (footnote 3, *Handbook of Chemistry and Physics*<sup>8</sup> or Figure 2), one can describe the humidity in terms of a frost (or dew) point. This is shown in Figure 3.

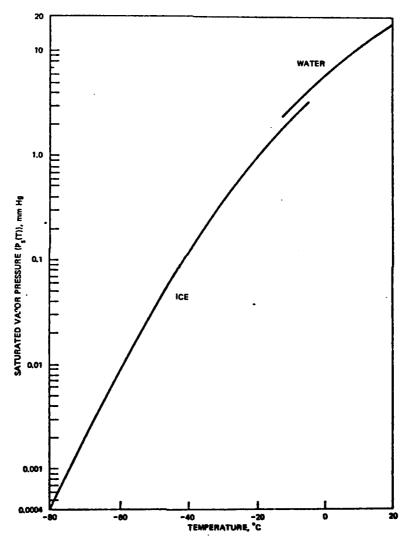


FIGURE 2. Temperature Dependence of the Equilibrium or Saturated Vapor Pressure of Pure Water.

<sup>&</sup>lt;sup>8</sup> The Chemical Rubber Co. Handbook of Chemistry and Physics. R. C. Weast and S. M. Selby, Ed., 47th ed. (1966), pp. D-105, 106.

It is interesting to note that if one overlays a transparency of Figure 3 on Figures 1a and 1b, some information on the probability of cloud formation emerges. If the frost point is greater than the ambient temperature, clouds will form.

The relative humidity at a temperature is the ratio of the water vapor pressure to the saturation pressure of water at that temperature  $(p_s(T))$ . If the calculated relative humidity is greater than unity, clouds will form. In the presence of clouds, contrail formation does little to increase the visibility (detection probability) of a missile. Therefore we are only interested in those portions of Figures 1 and 3 for which the frost point is lower than the ambient temperature.

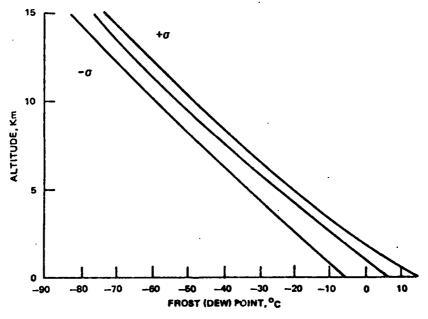


FIGURE 3. Frost (Dew) Point Temperature vs. Altitude from Humidity Model. (Fractional standard deviation is  $\pm 0.6$  of W or  $e_v$ .)

### COMPOUND MODEL

In order to move ahead from this stage of the model, two assumptions are necessary: (1) the relationship between the temperature and humidity models and (2) the shapes of the temperature and humidity probability distributions.

Independence of the temperature and humidity is assumed, and the shapes of the probability curves are assumed to be "triangular" as shown in Figure 4. These assumptions were made in lieu of readily accessible contradictory data.

Following this assumption, it is possible to calculate cumulative probabilities of any value of temperature and humidity and of the joint probability of any temperature-humidity pair. The probability of real interest is the joint probability that temperature will be below a specified value and that humidity will be above a certain value. The joint probabilities and relative humidities for this set are shown in Tables 2 through 15 for the altitude range of 2-14 km at both 40°N and 50°N lattitude. These tables were generated by the computer program given in the Appendix.

The number pairs enclosed by the rectangles in Tables 2 through 15 represent an 11 by 11 matrix of joint probabilities and relative humidities. The upper number in each pair is the joint probability; the lower, the relative humidity. The joint probability represents the probability that temperature is lower than the value in the far left column (outside the rectangle) and that humidity is greater than the value in the top row (outside the rectangle). The right-most column in each table is the probability that the temperature is less than the value in the left-most column. The lowest row in each table is the probability that the humidity (e<sub>v</sub> in mm Hg) is greater than the value in the top-most row. The second column in each table is the saturated vapor pressure, p<sub>s</sub>(T) or PSAT, associated with the temperature, TC, in the first

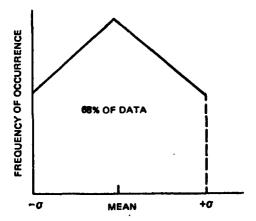


FIGURE 4. Assumed Probability Curve Shape for Temperature and Humidity.

column. The relative humidity is just the ratio  $e_{\rm v}/p_{\rm s}(T)$ . Regions in Tables 2 through 15 where the relative humidity is greater than unity correspond to natural cloud formation.

For example, if one looks at the central pair (the 6,6 matrix position) in the matrix of Table 2, the joint probability is 0.25; the relative humidity is 0.256 (or 25.6%). This pair corresponds to a temperature of 7.6°C (which has a saturated vapor pressure of 7.76 mm Hg) and an actual vapor pressure of  $e_v = 1.98$  mm Hg. There is a 0.5 probability that temperature is less than 7.6°C at this altitude and latitude and also a 0.5 probability that the humidity is greater than 1.98 mm Hg.

### CONCLUSIONS

A simple model for defining the atmospheric temperature and humidity at regions of operational interest for tactical missiles in the temperate zone of the earth's northern hemisphere has been described in this report. With this model one can define a probability distribution for temperature and humidity on any arbitrary day.

Definition of probabilities of these atmospheric variables may also be desirable for any particular day. In order to obtain appropriate values for this approach it will be necessary to computerize extensive records of atmospheric fluctuations and derive appropriate statistical and perhaps analytical approaches which are beyond the funding limits of the projects which supported this study.

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16.3	-138+02	.696+00	.650+00	.918-01	.109+00	.126.00	.403+00	.331+00	.266+00	. 208+00	.156+00	.230+00	.807	
14.2	20 +021.	.640+00	.859+60	.551+00	.497+00	.437+00	.371+00	.305+00 .185+00	.245+00	. 191+00	.144+00	.102+00	.742	
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1.0	.488+01	.222+00	.208+00	.191+00	.173+00	.152+00	.129+00	.106+00	.851-01	. 553+00	.499-01	.354-01	.258	
-1.2	2 .416+01	.167+00	.156+00	.305+00	.130+00	.114+00	.968-01	.795-01 .534+00	.591+00	. 499-01	.374-01	.763+00	.194	
-3.3	3 .354+61	.119+00	.111+00	.102+00	.921-01 .427+00	.810-01 .494+00	.551+00	.565-01	.454-01 .696+00	.354-01 .763+00	.266-01 .831+00	.898+00	.138	
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	-254+00	.554-00	.696+00	.640+00	.578+00	.508+00	.118+00	.184+01 .138+00	.162+00	.109+C1 .232+00	.167+00	.750+ GO .339+00	-862
	P SAT	-459+ 01	.396+ 61	.341+01	.293+01	.251+01	.215+61	.184+01	.157+01	.109+ 61	.907+00	.750+ 60	
	7C 0E6 C	?	4.	-3.8	-S.8	** 7	8· 6-	-11.8	-13.8	-15.8	-17.8	-19.8	
1													

NWC TP 3638, Revision 1

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	PROB TEMP :	.862	.807	•742	029.	.589	.500	.411	.330	.258	.194	.138	
	.322+00	.119+00	.111+00	. 102+00	.482+00	.810-01	.688-01 .691+30	.855-01	.100+01	.354-01	.260-01	.189-01	.138
:	.298+00	.167+00	.156+00	144+09	.130+00	.114+00	.968-01	795-01	. 926+00	. 112+01	374-01	.266-01 .165+01	. 194
· !	. 273+00	. 22 24 00	. 208+00	. 191+05 . 343+00	. 173+00	.152+05	. 587+00	. 106+00	.851-01	. 103+01	. 125+01	.354-01	.258
itude ure dity).	.249+00	.285+00	.268+00	.245+00 .313+00	.373+00	.195+00	.165+00	.136+00	.109+00	.851-01 .936+00	.114+01	.454-01 .136+01	.330
TABLE 4. Climate for 40°N Latitude 6.0 km Altitude 472.0 MB Pressure (Joint Probability/Relative Humidity).	.225+00	.354+00	.331+00	.283+00	.275+00 .337+00	.242+00	.206+00	.169+00	.136+00	.106+00	.795-01 .103+01	.565-01 .125+01	.411 .6T. EV
mate for ade 472.0 lity/Relat	.201+00	.431+00	.403+00	.253+00	.335+60	.295+00	.250+00	.205+00	.165+00	.129+00	.968-01	.688-01	. SOO
TABLE 4. Climate for 6.0 km Altitude 472.0 (Joint Probability/Rela	.177+00	.508+00	.187+00	.437+00	.394+00	.347+00	.295+00	.242+90 .457+00	.195+00	.152+00	.114+00	.9810-01	.589 IY THAT P
TAB 6.0 (Join	.153+00	.578+00	.546+00	.192+00	.229+00	.394+00	.335+00	.275+00	.221+00	.173+00	.130+00	.921-01 .847+00	.670 .589 .500 PROBABILITY THAT HUMIDITY
	.129+00	.40+00	.130+00	.551.00	.193+00	.437+00	.371+60	.305+00	.245+00	.191+00	.144+00	.102+00	.742
	.105+00	.696+00 .931-01	.450+00	.131+00	.546+00	.475+00	.403+00	.331+00	.266+00	.208+00	.156+00	.580+00	.807
	.604-01	.744+00	.849-01	.101+00	.120+00	.506+00	-431+00 -173+00	.354+00	.285+00	.222+00	.367+00	.119+00	-862
;	PSAT NA HG	.112+61	.947+60	00+964.	00 +899-	•558+ €0	00 +997	•388+ €0	.321+00	-266+00	.215+00	.180+ 60	
!	7C 9E6 C	-15.6	-17.4	-19.2	-21.1	14	-24.7	-26.6	-28.4	-30.3	-32.1	-33.9	

NWC TP 3638, Revision 1

		:		1	8.0 k	8.0 km Altitude 356.0 MB Pressure (Joint Probability/Relative Humidity)	ude 356.0 ility/Relati	8.0 km Altitude 356.0 MB Pressure Joint Probability/Relative Humidity)	ure lity).		·	:		
TC <b>DE6</b> C	PSAT RP. HG	.251-01	.326-01	.401-01	.476-01		.625-01	.702-01	.777-01	. 85 2-01	.927-01	.100+00	PROB TEM LT TC	ST dw
-28.6	.315+60	.744+00	.103+00	.127.00	.151.00	.508+00	.199+00	.354+00	.285+00	. 22 2 + 0 D	.167+00	.318+00	.862	
-30.3		.696+00 10-746. 00 +465.	. 123 +00	.152+00	.180+00	.475+00	.403+00	.331+00	.266+00	. 206+00	.156+00	.111+00	.807	
-32.0	.221+00	.640+00	.559+00	.551+00	.497.00	.437+00	.371+00	.305+00	.245+00	. 191+00	.144+00	.102+00	.742	
-33.7	.185+00	.136+00	.540+00	.497+00	.449+30	.394+00	.335+00	.380+00	.221+00	. 173+00	.130+00	.543+00	0.49	
-35 .4	.154+00	.508+00	.212+00	.437+00	.394+00	.347+00	.295+60	.242+00	.195+00	. 152+00	.114+00	.652+00	• 589	
-37.1	.126+ 00	.431+00	.403+00	371+00	.335+00	.295+00	.250+00	.206+00	.408+00	. 129+00	.968-01 .726+00	.785+00	• 500	
-38.6		.354+00	.378+00	.305+00	.450+00	.522+00	.205+00	.169+00	.136+00	.106+00	.795-01 .877+00	.948+00	.411	
-40.5	.873-61	.285+00	.266+00	.459+00	.221+00	.195+00	.165.00	.136+00	.109+00 .890+00	. 851-01	.039-01	.115+01	•330	
-42.2	.718-01	.349+00	.264+60 .453+60	.191+00	.173+00	.152+00	.129+00 .872+00	.106+00	.851-01 .106+01	. 119+01	.129+01	.354-01	.258	
-43.9	.590-C1	.167+00	.156+00	.680+00	.130+00	.935+00	.968-01	.795-01 .119+01	.639-01 .132+01	. 499-01	.374-01	.170+01	.194	
-45.0	.483-01	.519+00	.111+00	.102+00	.921-01 .986+00	.114+01	.130+01	.565-01	.454-01	.354-01	.192+01	.208+01	.138	
		.862	.607	2762	.670 .589	985.	.500	.411	.330	.258	.194	.138		

iitude ssure idity).	.238-0
40°N Lat 0 MB Pre ive Humi	.215-01
mate for ude 264.0 lity/Relat	192-01
TABLE 6. Climate for 40°N Latitude 10.0 km Altitude 264.0 MB Pressure (Joint Probability/Relative Humidity).	0-855. 10-215. 10-501. 10-601. 10-601. 10-
TAB 10.0 (Join	.146-01
	Ş

ر وور و	P SAT	.767-02 .998-02	.998-02	.123-01	.146-01	.169-01	192-01	.215-01	.238-01	. 261-01	.284-01	.307-01	PROB TEMP LT TC	18
-39 · C	.103+00	.103+ CO .744+00	.965-01	.119+00	.141+00	.508+00	.431+00	.354+00	.285+00	. 222+00	.167+00	.119+00	.862	
-40.6	13-498-	.696+00 .888-01	.650+60	.142.00	.169.00	.195+00	.403+00	.331+00	.266+00	. 208+00	.156+00	.355+00	.807	
-42.2	.721-61	00+040-	.138+60	.551+00	.497+00	.437+00	.371+00	.305+00	.245+00	. 191+00	.144+00	.102+00	-742	NWC
-43.8	.599- 11	.578+00	.540+00	.205+00	.449+00	.394+00	.325+00	.275+00 .358+00	.221+00	.435+00	.130+00	.512+00	.670	TP 3
-45.4	12-2690	.154+00	.475+06	.437.00	.394+00	.347+00	.295+00 .386+00	.242+00	.195+00	. 152+00	.114+00	.810-01	685•	638,
-46.9	.412-11	.431+00 .412-L1 .180+00	.403+00	.298+00	.335+00	.295+00 .410+00	.250+00	.522+00	.165+00	. 634+00	.968-01	.688-01	• 500	Revis
-46.5	.340-61	.354+00	.331+00	.305+00	.275+00	.242+00	.206+00	.633+00	.136+00	. 768+00	.795-01 .836+00	.904+00	.411	ion 1
-50.1	-280-01	.285+00	.357+00	.245+00	.522+00	.195+00	.165.00	.136+00	.109+00	. 651-01	.639-01	.110+01	•330	
-51.7	.229-61	.222+00 .335+00	.268+00 .435+00	.535+00	.636+00	.736+00	.129+00 .835+00	.937+00	.104+01	. 114+01	.124+01	.354-01	• 258	
-53.3	-188- C1	.167+00	.156+00	.144+00	.130+00	.903+00	.968-01	.115+01	.639-01	139-01	.151+01	.266-01	.194	
-54.9	.153-61	.153-01 .501+00 .111+00		.102+00 .802+00	.921-01	.110-01	.688-01 .125+01	.565-01 .140+01	.454-01 .155+01	. 354-01	.266-01 .185+01	.201+01	• 138	
		.862	.607	.742 PR	.670 .589 PROBABILITY THAT	.589 TY THAT H	.500 HUMIBITY	.411 .6T. EV	.330	.258	.194	.138		

NWC	TP	3638,	Revision	1

TABLE 7. Climate for 40°N Latitude 12.0 km Altitude 193.0 MB Pressure (Joint Probability/Relative Humidity).	.418-02 .475-02 .532-02	.508+00 .431+00 .354+00 .994-01 .113+00 .126+00	.475+00 .403+00 .331+00 .119+00 .135+00 .152+00	.437+00 .371+00 .305+00 .143+00 .163+00 .182+00	.394+00 .335+00 .275+00 .172+00 .196+00 .219+00	.347+00 .295+00 .242+00 .208+00 .236+00 .265+00	.295+00 .250+00 .206+00 .255+00 .255+00	.242+00 .205+00 .169+00 .306+00 .347+00 .389+00	.195+00 .165+00 .136+00 .372+00 .423+00 .473+00	.152+00 .129+00 .106+00 .454+00 .516+00 .578+00	.114+00 .968_01 .795-01 .556+00 .632+00 .707+00	.810-01 .688-01 .565-01 .682+00 .682+00 .776+00 .869+00	.589 .500 .411
TAB 12.0 (Join	47-02 .304-02 .361-02	.096+60 .640+00 .578+00 .587-01 .723-01 .858-01	50+00 .599+00 .540+00 34-01 .666-01 .103+00	.599+00 .551+00 .497+00 .845-01 .104+00 .124+00	60+00 .497+00 .449+00 62+00 .125+00 .149+00	75+UG .437+OG .394+OG 23+OG .151+OG .180+OG	03+00 .371+00 .335+00	31+00 .305+00 .275+00 81+00 .222+00 .264+00	.266+00 .245+00 .221+00 .220+00 .271+00 .321+00	.208+GD .191+DD .173+DD .268+OD .352+DD	.156+00 .144+00 .130+00 .328+00 .404+00 .480+00	.111+00 .102+00 .921-01 .463+00 .496+00 .589+00	010. 547. 5010
	P SAT .190-02 .247-	-46-8 .421-G1 .452-O1 .587-	-48.3 .351-C1 .541-01 .704-	-49.7 .295-C1 -450-01 .595	-51.2 .243-01 .783-01 .162+	-52.7 .201-61 .508+00 .475+	-54.2 .431+00 .403+	-55.7 .137-01 .354+00 .331+	-57.2 .12-01 .285+00 .266+	-58.7 .921-62 .206+00 .266	-60.2 .752-02 .167+00 .156	-61.7 .013-02 .310+00 .463+	.862 .60

NWC TM 3638, Revision 1

						* 3	******						
7C 0E6 C	P SAT	.471-03	.612-03	.753-03	.894-03	9	.118-02	.132-02	.146-02	. 160-02	.174-02	.188-02	PROB TEMP IS LT TC
-51·è	.225-01	.209-01	.272-01	.334-01	.3578+00	.506+00	.431+00	.354+00	.285+60 .646-01	. 22 2+ 00 . 71 0-01	.167+00	.836-01	.862
-53.3	.186-61	.250-01	.650+60	.599+00	.546+00	.551-01	.403+00	.331+00	.266+00	. 208+00	.156+00	.111+00	*807
-54.7	.156-61	.301-01	.391-01	.551+00	.497+00	.437+00	.371+00	.305+00	.245+00 .933-01	. 191+00	.144+00	.120+00	.742
-56.1	130-01	.578+0C	.546+68	.580-01	.449+00	.394+00	.335+00	.275+00	.221+00 .112+00	.173+03 .123+00	.130+00	.921-01	.670
-57.6	.108-61	.556+00 .438-01	.569-01	.437+00	.394+00	.347+00	.295+00	.123+00	.195+00	.152+00	.114+00	.175+00	.589
-59.0	-888- 62	.530-01	.403+00	.371+00	.335+00	.295.00 .117.00	.253+00	.206+00 .148+00	.165+00	. 129+00	.968-01	.212+00	• 500
1.00-	-731-62	.35.+00	.331+00	.305+00	.275+00	.242+00	.205+00	.180+00	.136+00	.219+00	.238+00	.565-01	.411
-61.9	-001-62	.285+00	.102+00	.125+00	.221+00	.195+00	.165+00	.136+00	.109+00	. 851-01	.639-01	.313+00	.330
-63.3	-492-C2	.222+00	.124+00	.191+00	.173+00	.152+00	.129+00	.106+00	.851-01 .296+00	. 325+00	.354+00	.382+00	• 258
-64.7	-405-02	.167+00	.156+00	.144+00	.130+00	.114+00	.968-01	.328+00	.639-01	. 499-01	.433+00	.266-01	.194
-66.2	.324-62	.119+00	.111+00	.233+00	.921-01 .273+00	.316+00	.359+00	.565-01	.454-01	.354-01	.532+00	.189-01	.138
	-	-862	.807	.742	0.670	589	.530	.411	.330	.259	.194	.138	

NWC TM 3638, Revision	NWC	TM	3638,	Revision
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	TEMP TC												
	PROB	.862	.807	.742	049.	.589	• 500	.411	.330	.258	.194	.138	
	.318+01	.119+00	.111+00	.102+00	.648+00	.795+00	.979+00	.121+01	.454-01	.354-01	.286-01	.189-01	.138
	.294+01	.333+00	.156+00	.144+00	. 130+00	.735+00	.968-01	.112+01	.139+01	.174+01	.374-01	.266-01	. 194
	. 270+01	. 22 24 03	. 208+00	. 191+00	. 551+00	.152+00	. 129+DD . 832+DD	.106+00	. 851-01	. 1664-01	. 243+01	.354-01	.258
itude ure dity).	-246+01	.285+00	.336+00	.245+00	.502+00	.195+00	.165+00	.939+00	.109+00	.851-01	.222+01	.454-01 .288+01	•330
TABLE 9. Climate for 50°N Latitude 2.0 km Altitude 795.0 MB Pressure (Joint Probability/Relative Humidity)	.222+01	.354+00	.331+00	.305+00	.453+00	.242+00	.206+00 .686+00	.169+00	.136+00	.132+01	.200+01	.565-01	.411 .6T. EV
Slimate for stude 795.0 bility/Relati	.193+01	.431+00	.403+00	.371+00	.335+00	.295+00	.252+00 .612+00	.205+00	.165+00	.129+00	.968-01 .179-01	.688-01 .232+01	.530 HUMIDITY
E 9. Clirkm Altitu	.175+01	.508+00	.475+80	.437+00	.356+00	.347+00	.539+00	.242+00	.195+00	.152+00	.157+00	.810-01 .204+01	
7.48L 2.0 1 (Joint	.151+01	.576+00	.540+00	.497+60	.308+00	.394+00	.335+00	.275+00	.221+00	.173+00	.130+00	.921-01 .176+01	.670 .589 ROBABILITY THAT
	.127+01	.640+00	.599+00	.551+00	.259+00	.437+00	.371+00	.305+00	.245+00	.191+60	.144+00	.162+00	.742 P.R
	.103+01	.096+00	.650+00	.599+00	.211+00	.475+00	.403+00	.331+00	.266+60	.208+60	.929+00	.111+00	.607
	.794+00	.901-01	.109+00	.440+00	.578+00	.508+00	.245+00	.354+00	.285+00	.222+00	.167+06	.119+00	-862
	PSAT An HG	10+188.	.728+ C1	.599+ 61	.490+61	*******	.324+01	.262+01	10+115.	.169+01	.111+61	07 +559-	
i	7C P	9.8	4.7	m ••	:	-1.7	-4.5	-7.3	-10.1	-12.9	-15.7	-16.5	
						19							

NWC	TM	3638,	Revision	1
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		18		i	NWC	1M 3	638,	Kevisi	ion i					
		16 MP												
		PROB	.862	.807	.742	.670	.589	• 500	.411	•330	.258	.194	.138	
		.102+01	.351+00	.427+00	.152+00	.921-01	.810-01	.122+01	.150+01	.200+01	.258+01	.335+01	.437+01	.138
† ; ;		.940+00	.167+00	.156+00	.144+00	.130+00	.114+00	.968-01	.144+01	.639-01	.239+01	.374-01	.266-01	. 194
•		. 864+00	. 22 2+ 00	. 20 8+00	. 191+00	. 173+00	.152+00	. 129+00	. 133+01	. 170+01	. 219+01	. 285+01	.354-01	\$52.
ititude sure idity).		.788+00	.285+00 .272+00	.331+00	.245+00	.221+00	.195+00 .745+00	.165+00	.136+00	.155+00	.200+01	.260+01	.339+01	•330
· 50°N La ) MB Pres tive Hum		.712+00	.354+00	.331+00	.365+00	.275+00	.242+00 .673+00	.206+00 .855+00	.169+00	.136+00	.106+00	.234+01	.565_01	.411 .67. EV
Climate for 50°N Latitude titude 616.0 MB Pressure ability/Relative Humidity).	**************************************	.635+00	.431+00	.403+00	.325+00	.403+00	.295+00	.250+00	.975+00	.165+00	.129+00	.209+01	.688-01	. SDO humisity
10. Toba	EV. BR.	.559+00	.508+00	.235+00	.437+00	.352+00	.347+00	.295+00	.242+00 .358+06	.195+00	.152+00	.114+00	.240+01	. 589 THAT
TABI 4.0 (Join	* > U	.483+60	.578+00	.540+00	.497+00	.449+00	.394+00	.335+00	.275+00	.951+00	.173+00	.136+00	.921-01	.67C ROBABILITY
		.407+00	.140+00	. 171+00	.551+00	.256+00	.437+00	.489+60	.305+00	.245+00	.191+00	.144+00	.102+00	.742 9
		.330+00	.696+00	.450+00	.599+00	.540+00	.475+60	.397+00	.331+00	.651+60	.208+00 .639+00	.156+60	.111+60	.807
ļ		.254+00	.744+00 .874-01	.238+61 .107+00	.131+00	.159+ 01 .160+00	.508+00	.431+00	.354+00	.500+00	.222+00	.437+00	.119+00	.862
		PSAT MP H6	.289+ 61	.238+61	.195+41		10+01.	.432+ 60	.652+ 60	იე +8ე <b>5</b> •	.394+60	•304+€0	.233+ CO	
	٠	1C DEG C	9-	9.8	-11.1	-13.7	-16.2	-18.5	-21.3	-23.6	-26.4	-29.0	-31.5	•

NWC TP 3638, Revision 1

SI .			NWC	TP 3	3638,	Revis	sion 1					
TEMP						_		_			_	
PROB LT	-862	.807	.742	.670	.589	• \$00	.411	.330	•258	.194	.138	
.322+00	.401+00	.501+00	. 102+00	.921-01	.101+01	.129+01	.565-01	.212+01	.354-01	.356+01	.189-01	.138
.298+00 .322+00	.167+00	.156+00	.144+00	.130+00	.114+00	.968-01	.152+01	.196+01	.253+01	.374-01	.430+01	. 194
. 273+00	. 340+00	. 208+09	. 191+00	.173+00	.152+09	. 129+00	.10000	. 18 0+01	. 233+01	. 499-01	.354-01	•258
.153+00 .177+00 .201+00 .225+00 .249+60 .273+00	.285+00 .310+00	.388+00	.245+00	.616+00	.195+00 .782+00	.165+00 .129+00 .996+00 .109+01	.136+00 .128+01	.109+00	.851-01	.639-01	.454-01	•330
.225+00	.354+00	.331+00	305+00	.275+00	.242+00	.206+00	.169+00	.136+00	.192+01	.249+01	.565-01	.411 .67. EV
.201+00	.431+00	.403+00	.371+00	.335+00	.630+00	.250+00 .803+00	.206+60	.165+00	.129+60	.968-01	.291+01	.530 HUMIÐITY
.177+00	.508+00	.475+00	.437+00	.394+00	.347+00	.295+00	.242+00	.195+00	.152+00	.196+01	.256+01	.589 FY THAT P
	.193+00	.546+00	.299+00	.378+00	.394+00	.335+00	.275+00 .782+00	.101+01	.173+00	.130+00	.921-01 .221+01	.67C .589 Phobability THAT
.129+00	.160+00	.201+00	.252+00	.497+00	.437+00	.371+00	.305+00	.245+00	.191+00	.144+00	.162+00	.742 Pt
.804-01 .105+00	.130+60	.650+00	.599+50	.540+60	.475+00 .326+00	.473+00	.331+00	. 266+00 . 0 28+00	00+907* 00+068*	.156+60	.119+00 .111+00 .110+01. 151+01	.807
.804-01	-803+ CG -100+00	.696+00	.511+ 60 -156+00	.404+ 60 -199+00	.506+00 .252+00	.431+00	.354+00	.285+00 .529+00	.222+00	.964-61 .896+00	.692- C1 .110+011	.862
FSAT NF H6	. 03 + €0 0+	07 +240.	.511+ 60	.404+ 60	-319+00	.250+ LG	.196+ 00	30 +251.	.118+ 00	13-796-	.692- نا	-
7C 9EG C	10.1	-21.5	-23.4	-26.2	-28.5	-30.6	-13.2	-35.5	-37.9	-+0.2	-42.5	

TABLE 11. Climate for 50°N Latitude 6.0 km Altitude 472.0 MB Pressure

(Joint Probability/Relative Humidity).

NWC	IP	3638,	Revision	

	S I			NWC	TP 3	638,	Revisi	ion 1					
	TE MP TC												
	PROB	. 662	.807	.742	.670	.589	.500	.411	•330	•258	.194	.138	
	.100+00	.119+00	.111+00	.102+00	.921-01	.923+00	.118+01	.565-01	.454-01	.354-01	.320+01	.189-01	.138
	.927-01	.167+00	.156+00	.144+00	.130+00	.114+00 .654+00	.968-01	.795-01 .139+01	.179+01	.232+01	.374-01	.394+01	. 194
	. 852-01	. 22 2 + 00	. 208+00 . 389+00	. 191+00	.173+00	.152+00	. 129+03	.128+00	. 651-01 . 165+01	.213+01	. 277+01	.354-01	•258
iitude ure dity).	10-222	.285+G0 .283+G0	.266+00	.245+00	.221+00	.195+00	.912+00	.130+00	.150+00	.851-01	.639-01 .252+01	.330+01	.330
TABLE 12. Climate for 50°N Latitude 8.0 km Altitude 356.0 MB Pressure (Joint Probability/Relative Humidity).	.702-01	.354+00	.331+00	.305+00	.275+00	.242+00	.206+00	.169+00	.136+00	.106+00	.795-01 .225+01	.298+01	.411 .6T. EV
TABLE 12. Climate for 50 8.0 km Altitude 356.0 ME (Joint Probability/Relative	.626-01	.431+00 .228+00	.403+00	.360+00	.335+00	.295+30	.253+00 :735+00	.941+00	.165.00	.129+00	.204+01	.688-01 .265+01	. SOO HUMIDITY
FABLE 12. Climate for 8.0 km Altitude 356.(Joint Probability/Relative, mm H6	.551-01	.201+00	.475+00 .252+00	.437+00	.394+00	.347+00	.295+00	.242+00 .828+00	.195+00	.152+00	.114+00	.810-01	.539 THAT
TABL 8.0 (Join	.476-01	.575+00	.540+00	.497+00	.449+00	.438+00	.335+00	.275+00	.221+00	.173+00	.130+00	.921-01 .202+01	.670 kobability
	.401-01	.640+00	.183+00	.551+00	.291+00	.437+00	.371+00	. \$03+00	.245+00	.191+00	.144+00	.102+00	.742
	.326-01	.119+00	.650+00 149+00	.599+00	.540+00	.300+00	.403+00	.331+00	.630+00	.208+00 .815+60	.156+00	.111+00	.607
	.251-01	.744+00	.696+30	.640+00	.578+00 .182+00	.231+00	.431+00	.354+00 .665-01 .377+00	.285+00	.627+00	.167+00	.119+00	298.
	F SAT	.275+ 60	•219+ €0	.174+00	.138+ 00	00+601.	.852- 01	1ù-868-	.517-01	19-004-	.308- 61	.236-01	
	16 DE6 C	-30.0	-32.1	-34.3	-36.4	-38.0	-40.7	-42.9	-45.0	-47.2	-49.3	-51.5	

	SI			NWC	IM 3	,030	Revis	ion i					
	TEMP TC												
	PROB	.862	.807	.742	.670	.589	.500	.,1	.330	.258	.194	•138	
	.307-01	.119+00	.111+00	.102+00	. 553+00	. 810-01	.688-01 .891+00	.565-01	.454-01	.354-01	.266-01	.318+01	.138
	.284-01	.167+00	.156+00	.144+00	. 3 11+00	.114+00	.968-01 .624+00	.795-01 .105+01	.639-01	.499-01	.226+01	.266-01 .294+01	. 194
	. 261-01	. 222+00	. 208+00	. 191+00	. 173+00 . 470+00	. 152+00	. 129+00	. 106+00	. 124+01	. 160+01	. 208+01	.354-01	.258
rtitude ssure idity).	.236-01	.285+U0 .216+G0	.266+60 .27u+00	.245+00	.221+00 .428+00	.195+00	.691+00	.130+00	.109+00	.851-01	.639-01	.454-01	.330
TABLE 13. Climate for 50°N Latitude 10.0 km Altitude 264.0 MB Pressure (Joint Probability/Relative Humidity).	.215-01	.354+00	.331+00	.305+00 .307+00	.387+00 387+00	.242+00	.206+00	.169+00 .797+00	.136+00	.132+01	.795-01	.565-01	.411 .6T. EV
13. Climate for n Altitude 264. robability/Relat	.192-01	.431+00	.403+00 .218+00	.371+00	.335+00 .345+00	.295+00 .438+00	.250+00 .557+00	.205+00	.165+00	.129+00	.963-01 .153+01	.688-01 .199+01	.500 HUMIDITY
E 13. Cl	.169-01	.508+00	.192+00	.437+00	:394+88	.347+00	.490+00	.242+00	.195+00	.152+00	.114,00	.810-01 .175+01	.679 .589 08ABILITY THAT
TABI 10.0 (Join	.146-01	.578+00 .132+00	.166+30	.497+00	.263+00	.394+00	.335+00	.275+30	.221+00	.173+00 .895+00	.130+00	.921-01 .151+01	.670 kobabili
	.123-61	.640+00	.599+00	.551+00	.221+00	.437+00	.371+00 .356+00	.305+00	. 245+00 . 585+00	.191+66	.144+00	.102+00	.742 p
	.996-02	.696+00 .906-01	.113+00	.599+ŭ0 .142+ŭ0	.540+00 .180+00	.475+00 .228+00	\$50+00°	.331+00	.266+00	.208+00 .613+00	.156+60	.111+60	.607
	.767-02	.244+00	.696+60 .872-01	.110+60	.555-C1 -578+00	.564+00	.431+00	.285+00	.216-C1 .365+00	.222+30	.167.00	.119+00	.862
	P SAT	110+06	10-684	.700-61	15-555-	.438-(1	.344-11	.270-61	.216-01	.163-61	.126-61	59 - S96°	
	1C DEG C	-38.4	7-07-	7.24-	7.77-	1.01-	1.81-	-50.4	-55.4	-54.4	-56.4	-53.4	

s		]	NWC	TM 3	638,	Revisi	on 1					
TEMP 1												
PROB T	298.	.807	272	029	.589	200.	.411	330	.258	194	.138	
											<del></del> -	ī
.760-02	.119+00	.111+00	.102+05 .219+00	.921-01 .275+00	.810-01 .347+00	.685-01	.565-01	.454-01 .713+00	.354-01	.116+01	189-01	.138
.703-02	.167+00	.156+00	.144+00	.130+00	.114+00	.968-01	. 795-01 . 517+00	.6 60+00	.499-01	.374-01	.266-01	. 194
• 64 6-02	.222+00	. 208+00	.191+09	. 173+00	. 152+00	.129+00	.106+09	. 651-01	. 064-01	. 100.01	. 354-01	.258
.589-02	.285+00 .108+00	.266+00	245+00	.221+00	.195+00	.165+00	.130+00	.553+00	.709+00	.639-01	.454-01	.330
.532-02	.354+00	.331+00	305+00	.275+00 .192+00	242+00	307+00	.391+00	136+00	.106+00	.795-01	.565-01	.411 .6T. EV
. 475-02	.431+00	.403+00	.371+00	.335+00	.295+00 .217+00	.250+00	.349+00	.165+00	.129+00	.968-01 .737+00	.955+00	.500 HUMIDITY
.418-02	.508+00	.475+00	.437+00	.394+00	.347+00	.295+00	.307+00	.195+00	.152+00	.114+00	810-01	. 589 THAT
.361-02	.578+00	.540+00	.104+00	.130+00	.394+00	.335+CD .209+00	.265+00	.221+00 .339+00	.435+00	.130+00	.921-01	.67C PROBABILITY
.304-02	.640+00	.599+00	.551+00 .874-01	.497+00	.437+00	.371+00	.305+00	.245+00	.191.00	.144+00	.102+00	.742 PH
.247-02	.c96+00 .455-01	.650+00 .567-01	.299+60	.540+00	.113+00	.403+00	.181+00	.232+66	.206+60	.156+00	.111+50	. 807
.190-02 .247-02	.543-61 .350-01	.696+00	.346-01 .540-01	.578+00 .687-01	.219-01 .566-01	.431+00 .116+00	.136-C1 .354+00 .331+00	.178+00	.222+00	.167+00	.119+00	-862
PSAT NV X6	19-295	.436-61	.346-01	.277-01	.219-61	173-01	.136-61	12-701.	.631-02	.644-62	.498-62	
TC	9.77-	-40.5	-48.3	-50.2	-52.0	-53.9	-55.8	-57.6	-59.5	-61.4	-63.2	

NWC 7	ГМ	3638.	Revision	1
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					14.0 (Joint	Prob	Ititude 141.0	MB Pres	aruae sure Jity).				! :
7C DEG C	7	.471-03	.612-03	.753-03	.894-03	.104-02	.118-02	.132-02	.146-02	. 160-02	.174-02	.188-02	PROB TEMP I LT TC
7.87-		.343-61 .137-01	.178-61	.220-01	.261-01	.508+00	.431+00	.354+00	.285+00	. 222+03	.167+00	.119+00	.862
50.2		10-071- 10-075-	.650+00	.599+00	.540+00	.475+00	.403+00	.331+00	.266+00 .528-01	. 208+00	.156+00	.681-01	.807
-52.6		.222-61 .212-01	.599+00	.551+00	.497+00	.437+00	.371+00	.305+00	.245+00	. 721-01	.144+00	.102+00	• 742
-53.7		.178-01 .265-01	.540+00	.497+00	.449+00	.583-01	.335+00	.275+00	.221+00 .821-01	. 173+09	.130+00	.921-01	029.
-55.5	.142-61	.506+00	.475+00	.437+00	.394+00	.347+00	.295+00 .833-01	.930-01	.195+00 .103+05	. 152+00	.114+00	.133+00	• 589
-57.2		.113-01 .431+00	.403+00	.371+00	.335+00	.295+00	.250+60 .105+00	.206+00	.185+00	. 129+00	.966-01	.688-01	• 500
-59.0	.691-C2	.354+00	.331+60	.305+00	.100+00	.242+00	.205+00 .132+00	.169+00	.130+00	. 180+00	.795-01 .195+00	.211+00	.411
60.7	.702-62	.285+00 .670-01	.206+00 .871-01	.245+00	.221+00	.195+00	.165+00	.136+00	.109+00	. 228+00	.639-01	.454-01	.330
-62.5	.551-uz	.222+00	.208+00	.191+60	.173+00	.152+00 .188+00	.129+00	.239+00	.851-01	. 290+00	.499-01	.354-01	.258
-64.2	-431-02	.167+00	.156+00	.144+00	.130+00	.114+00	.968-01	.795-01 .306+00	.639-07	. 449-01	.374-01	.266-01	.194
-66.0		.335-C2 .140+00	.111+00	.102+00	.921-01	.810-01 .309+00	.688-01	.393+00	.454-01	.354-01	.519+00	.561+00	.138
		.862	208*	.742 PR	.670 .589 OBABILITY THAT	Į.	.500 HUMIDITY	.411 .6T. EV	.330	\$52°	194	•138	

## Appendix COMPUTER PROGRAM FOR GENERATING PROBABILITY TABLES

```
2*
           C+++ PROGRAM TO CALCULATE CLIMATE AT 40 AND 50 DEG NORTH LATITUDE
           C****CORRECTED VERSION, 4 JAN 1979
  4.
  5*
                   Y IS ALTITUDE, KM
                  XLAT IS LATITUDE, DEG N
PATM IS ATMOSPHERIC PRESSURE IN MB
  6+
 7*
  8*
 9 *
                   DIMENSION H(11), PH(11), PT(11), PJ(11), RH(11), PHH(11), PTT(11)
                5 READ(5, 100, END=75) Y, XLAT, PATM
10*
11+
                  WRITE(6,200)XLAT,Y,PATM
12*
                   IF(XLAT-LT-50.) 60 TO 10
13*
          C
14*
                   FOR LAT = 50 DEG N
15+
16+
                   TEMP=12.95-8.774+Y+.2738+Y++2.
17+
                   TE = 10.3-0.7*Y+.0167*Y**2.
18*
                  $160 = 6.
19.
                   S16L = 4.
20+
                   TU= TEMP+TE+SIGL
21.
                   TL = TEMP-TE-SIGU
22+
                   60 TO 20
              FOR LATITUDE = 40 DEG N
10 TEMP = 28.56-10.618+Y+.3168+Y**2.
TE = 8. - .56+Y +.0153+Y**2.
SIGU = 5.
23*
24+
25*
26.
                  S16L = 3.
27+
                  IF(Y.GT.14.) GO TO 15
TU = TEMP + TE + SIGL
28*
29*
30±
                  TL = TEMP - TE - SIGU
31 *
                   60 TO 2C
              15 TU = TEMP + TE + SIGU
TL = TEMP - TE - SIGL
32*
33*
34.
                  CALCULATE HUMIDITY
35*
              20 1f(Y.6T.10.) 60 TO 21
36*
                  H = 10.4+(3.7 - .192+Y)
37-
                  60 TO 22
38*
               21 H = 10.**(4.13 - .235*Y)
              22 EV = PATM * W/622000.
EVHG = EV*.7502
39*
40+
41*
                  EVHGU = 1.6+EVHG
                  EVH6L = .4*EVH6
CALCULATE TEMPERATURE STATISTICS
BT = (TU - TL)/.72
AT = TL - .14*BT
42*
43*
44*
45*
          Ç
                  CALCULATE HUMIDITY STATISTICS
BH = -(EVHGU - EVHGL)/.72
AH = EVHGU - .14*BH
46*
          C
47+
48*
49*
                  CALCULATE JOINT PROBABILITIES AND RELATIVE HUMIDITIES
50*
                  PH(1) = .8625
                  PHH(1) = .86
DO 30 I = 1,11
51*
52±
53*
                  H(I) = AH + PHH(I)*BH
                  IF(I.LE.5) DED =(0.825*(1-1) +5.6)*.01
IF(I.6T.5) DED =(0.825*(10-1) + 5.6)*.01
54*
55*
56*
                  PH(I+1) = PH(I) - DED
                  PHH(I+1) = PHH(I) - .072
57*
              30 CONTINUE
58*
59*
                  WRITE(6,210)
60+
                  WRITE(6,220) (H(1),1=1,11)
```

```
61+
                PT(1) = .8625
                PTT(1) = .86
62*
               00 40 J=1,11
TC = AT + PTT(J)+BT
63*
64*
                T = TC + 273.
65+
66*
                IF(T.LT.258.) 60 TO 520
67*
           510 VPS =(((.135601£-7*T-.151036E-4)*T+.00618156)*T-1.07005)*T+64.058
68*
                60 TO 530
69*
           520 VPS=(((.538009E-05-.473762E -08*T)*T-.00243188)*T+.545827)*T-50.27
7C+
               189
           530 VPS = 10.**VPS
714
72*
               PH(1) = .8625
73*
               DO 35 I =1,11
74*
               PJ(I) = PH(I)*PT(J)
75±
               RH(I) = H(I)/VPS
764
            35 CONTINUE
               WRITE(6,230)TC,(PJ(I),I=1,11),PT(J)
WRITE(6,240)VPS,(RH(I),I=1,11)
IF(J-LE-5) DED =(0.825*(J-1) +5.6)*.01
77*
78*
79*
80+
               IF(J.GT.5) DED =(0.825+(10-J) + 5.6)+.01
               PT(J+1) = PT(J) - DED
PTT(J+1) = PTT(J) - .072
81*
82*
83*
            40 CONTINUE
84*
               WRITE(6,250) (PH(I),I=1,11)
85*
               WRITE(6,260)
86+
               60 TO 5
87*
            75 CALL EXIT
88*
           100 FORMAT()
           89*
90*
91+
92*
93*
94*
95*
96.
           250 FORMAT(1H0T15,11F8.3)
260 FORMAT(1H T40, PROBABILITY THAT HUMIDITY .GY. EV")
97*
98+
               END
```

## END

# DATE FILMED G-80

DTIC